

LIEGE UNIVERSITY
Urban & Environmental Engineering
Structural Engineering

USER'S MANUAL FOR SAFIR (version 2025)
A COMPUTER PROGRAM FOR ANALYSIS OF STRUCTURES
SUBJECTED TO FIRE

Part 2: thermal calculations

by

Jean-Marc Franssen* & Thomas Gernay**

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* info@safirsuport.be

** safir@uliege.be

This document explains the introduction of data for thermal calculation with the software SAFIR developed at the University of Liege for the simulation of building structures subjected to fire.

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1. Detailed description of the input file for thermal analyses

SERIES 1: COMMENTS

A. Multiple cards (can be 0)

As many lines as required may be introduced by the user at the beginning of the file to comment the content of the file. These comments will not influence in any manner the results of the calculation. They will help understand what the file is about, which may be particularly useful if the file is found and opened several years after it has been created. Experience shows that the users tend to neglect the comments, relying on the characters that are used in [filename] to differentiate several calculations made for a project. Using extensively the possibility of introducing detailed comments in the file is nevertheless highly preferable because it allows reporting much more information.

B. 1 card

1 blank line to indicate that the comments are finished.

SERIES 2: QUANTITY OF NODES

1 card

NNODE, *nnode*

- NNODE

Command.

- *nnode*

Quantity of nodes of the model. Minimum value is 3. There is no maximum value.

```
This file has been created as an example for the users manual of SAFIR
Date: 01/02/2022
Author: Jean-Marc Franssen
This model has 16 nodes
```

```
NNODE    16
```

SERIES 3: QUANTITY OF DIMENSIONS

1 card

NDIM, *ndim*

- NDIM

Command.

- *ndim*

Quantity of dimensions of the model.

- *ndim* = 2 for 2D models.
- *ndim* = 3 for 3D models.

SERIES 4: DEGREES OF FREEDOM

1 card

NDOFMAX, 1

- NDOFMAX

Command.

- 1

This card indicates that the maximum quantity of degrees of freedom for the nodes is 1 in a thermal analysis. The degree of freedom is the temperature of the node.

SERIES 4b (optional): SOLVER

1 card (optional)

SOLVER, *solvetype*

- SOLVER

Command.

- *solvetype*

SYM: SAFIR will compute and solve a symmetrical stiffness matrix or conductivity matrix.

NOSYM: SAFIR will compute and solve a non-symmetrical conductivity matrix.

solvetype = NOSYM only makes sense in thermal analyses when the model contains one or several VOIDS, in which case it is recommended because it will facilitate convergence and reduce instabilities which have been observed in some VOIDS with complex shapes. For all other problems, NOSYM should not change the results but should be slower.

solvetype = SYM is considered if this series is not present.

SERIES 5 (optional): CORES OF THE CPU

1 card (optional)

NCORES, *ncores*

- NCORES
Command.
- *ncores*

Quantity of cores of the CPU of the computer used by matrix solver. The default value is 1, in which case this card may be omitted.

This card can be used to force SAFIR to use more than 1 core if present on the computer. Experience has shown that using more than 1 core hardly reduces the duration of the runs with the present versions of Pardiso and Windows. This card can thus be omitted as a common practice. The possibility of using the card has nevertheless been given to allow users to perform their own tests on their particular system, and to offer the possibility of working with more than 1 core in the future if new releases of Pardiso and/or Windows show a difference of run time as a function of the number of cores mentioned in this card.

SERIES 6: THERMAL CALCULATION

A. 1 card, choice between two possible settings.

COMMAND

- COMMAND = TEMPERAT

is used for a normal thermal calculation from time $t = 0$ to a final time to be defined by the user (see *uptime* in SERIES 21).

- COMMAND = RESTARTT

is used if a previous thermal analysis has been made and a new thermal analysis must be restarted from a restart time t_i (to be defined by the user) up to a final time. The temperature field at time t_i is taken from the previous analysis. The new analysis can be performed either on the same structure as the previous analysis or on a new structure that is only one part of the previous structure.

The first possibility is used if the structural analysis shows that the thermal analysis had been stopped too early.

The second possibility is used, for example, to consider the fact that some layers of concrete or of protective material have fallen off the structure (what part has fallen off and at what time has to be decided by the user).

The next 3 cards, B, C and D are present only if RESTARTT has been entered in card A.

If TEMPERAT has been entered in card A, then go directly to card E.

B. 1 card

FIRSTFILE, *filename*

- FIRSTFILE

Command.

- *filename*

Name (comprising the file name and the file type) of the ".OUT" file where the results of the previous thermal analysis have been written. This file must be present in the same folder as the input file of the thermal analysis.

C. 1 card

FIRSTTIME, *time*

- FIRSTTIME

Command.

- *time*

Time (in seconds) when the second analysis will start. The temperatures will be read from the first analysis and used as initial values for the second analysis.

D. 1 card, choice between two possible settings.

COMMAND

- COMMAND = MATCHNODES

is used if the second structure is exactly the same as the first one or if its nodes were the first nodes of the first structure. In that case, the initial temperature at each node in the second structure is taken as the temperature at the same node in the first structure.

- COMMAND = MATCHCOORD

allows considering that the initial temperature at each node in the second structure is taken as the temperature of the node of the first structure with same coordinates. This possibility is used if some among the first nodes of the first structure have been deleted when creating the second structure.

E. 1 card

TETA, *teta*

- TETA

Command.

- *teta*

Parameter for the time integration. $0 < \textit{teta} \leq 1$. Values of *teta* close to 0 will force SAFIR to perform the time integration in a nearly explicit manner, whereas *teta* = 1 will lead to a fully implicit integration. *teta* = 0.9 has been used consistently by the developers in their own applications.

F. 1 card

TINITIAL, *tinitial*

- TINITIAL

Command.

- *tinitial*

Temperature (in degree Celsius) in the model at time $t = 0$, usually taken as 20°C.

SERIES 7: CONVERGENCE STRATEGY

1 card, optional, choice between two possible settings.

- COMEBACK, *timestepmin*
COMEBACK
Command.
timestepmin
Minimum value for the time step in case of comeback.
- NOCOMEBACK
Command.

Notes :

- 1) If NOCOMEBACK is chosen, the simulation is stopped if convergence is not reached after 18 iterations.
If COMEBACK is chosen, when the convergence is not reached after 6 iterations, time is reset at the last converged step and the simulation restarts from there with a time step divided by 2. The division of the time step goes on until the time step is smaller than *timestepmin*
- 2) This card is optional. If it is not present, NOCOMEBACK will be applied

SERIES 8: DIAGONAL CAPACITY

1 card (optional)

DIAG_CAPA

Command.

If this card is present, the capacity matrix of the finite elements is made diagonal. This reduces skin effects which can appear in the direction of non-linear temperature gradients.

If this optional card is not present, the full capacity matrix is used (as was the case in all versions of SAFIR until and including SAFIR 2019).

Utilisation of this capability is recommended and the diagonalised version may become the default setting in the future.

SERIES 9: STORAGE OF RESULTS

A. 1 card (optional), choice between 8 possible settings.

COMMAND

- `COMMAND = MAKE . TEM`
stores the average temperature of the elements for a subsequent structural analysis. The section analysed here is the cross section of a beam.
- `COMMAND = MAKE . TEMHA`
is similar to `MAKE . TEM`, but the fire is a localized fire as described in Annex C of EN 1991-1-2 (equation C.4, flame impacting the ceiling – Hasemi fire), see Section 2. The sections analysed here are the cross section of a beam.
- `COMMAND = MAKE . TEMLF`
is similar to `MAKE . TEM`, but the fire is a localized fire as described in the RFCS research report LOCAFI, see Section 2. The sections analysed here are the cross section of a beam.
- `COMMAND = MAKE . TEMCD`
is similar to `MAKE . TEM`, but the effects of the fire are described in a transfer file computed by a CFD analysis (made, for example, with FDS). The sections analysed here are the cross section of a beam.
- `COMMAND = MAKE . TEMTR`
is similar to `MAKE . TEM`, but the fire is a travelling fire described as “simple analytical model” in the RFCS research report TRAFIR, see section 3. The sections analysed here are the cross section of a beam.
- `COMMAND = MAKE . TSH`
stores the temperature of the first $nnode/2$ nodes for a subsequent structural analysis. The section analysed describes the temperature evolution across the thickness of a shell element.
- `COMMAND = MAKE . TSHHA`
is similar to `MAKE . TSH`, but the fire is a localized fire as described in Annex C of EN 1991-1-2 (equation C.4, flame impacting the ceiling – Hasemi fire), see Section 2. The sections analysed describe the temperature evolution across the thickness of shell elements.
- `COMMAND = MAKE . TSHCD`
is similar to `MAKE . TSH`, but the effects of the fire are described in a transfer file computed by a CFD analysis (made, for example, with FDS). The sections analysed describe the temperature evolution across the thickness of shell elements.

If MAKE . TEM or MAKE . TSH has been entered in card A, then

The next 2 cards, B and C are omitted

else

A file called “*hasemi.txt*” (for MAKE . TEMHA¹ or MAKE . TSHHA), a file called “*locafi.txt*” (for MAKE . TEMLF), a file called “*cfid.txt*” (for MAKE . TEMCD or MAKE . TSHCD), or a file called “*trafir.txt*” (for MAKE . TEMTR) must be present in the same folder as the input file. This file describes the position of the fire in the structure and its thermal characteristics, such as the rate of heat release. The structure of these files is described in Section 2.

B. 1 card (optional)

filename

This is the complete name of the input file of the structural analysis (maximum 20 characters).

Note: the input file describing the structural analysis must be present in the same folder as the input file for the thermal analysis when the thermal analysis is run. If the structural analysis is 2D, gravity must be pointing downward the **y** axis (i.e. Y is vertical upward). If the structural analysis is 3D, gravity must be pointing downward the **z** axis (i.e. Z is vertical upward).

C. 1 card (optional)

COMMAND, *ielemtype*

- COMMAND, choice between two possible settings.

COMMAND = BEAM_TYPE if the temperatures are determined in a beam section.

COMMAND = SHELL_TYPE if the temperatures are determined in a shell section.

- *ielemtype*

The number in the structural input file of the section type (beam or shell) treated in this thermal analysis.

¹ The name of the file is “*hasemi.txt*”, even if the function HASEMI_FR is used in series 16.

SERIES 10: MATERIALS

A. 1 card

NMAT, *nmat*

- NMAT

Command.

- *nmat*

Quantity of different materials. If two materials have the same name but different thermal properties (such as, e.g., the emissivity) or different mechanical properties (such as, e.g., the yield strength), this makes two different materials.

SERIES 11: ELEMENTS

A. 1 card

ELEMENTS

Command.

B. 1 card

SOLID, *nsolid*

- SOLID

Command.

- *nsolid*

Quantity of SOLID elements in the model. Thermal calculations are based on SOLID elements.

C. 1 card

NG, *ng*

- NG

Command.

- *ng*

Quantity of integration points in each direction in the elements. Not less than 1, not greater than 3. 2 has been used consistently by the developers in their own applications.

D. 1 card

NVOID, *nvoid*

- NVOID

Command.

- *nvoid*

Quantity of internal voids, also called internal cavities, i.e., areas in the section where there is no material but there is heat transfer between the walls that make the cavity by convection and by radiation. 0 must be typed if there is no cavity in the model.

Note: Computation of the view factors in cavities may take some time, especially in 3D models. When a model is run for the first time, a file with the file type “Fij” is created in which the views factors are written. If a second run is made on the same geometry (changing, for example, the boundary conditions), the view factors will be read from this file, which will save CPU time. If the geometry of the model is changed, either the name of the input file must be modified, or the Fij file must be deleted.

E. 1 card (optional)

This card is present only if $nvoid \neq 0$

FRTIERVEROID, *nfrontiervoid*

- FRTIERVEROID
Command.
- *nfrontiervoid*

Maximum (for all the voids of the section) quantity of surfaces (i.e. sides of finite elements) enclosing the internal voids.

For example, if a section has 2 cavities and one of them is enclosed by 50 surfaces, whereas the second one is enclosed by 30 surfaces, then *nfrontiervoid* is equal to 50.

If one finite element has two of its sides that define a void, this makes two different surfaces.

F. 1 card

END_ELEM

Command.

The input file, starting after the blank line that follows the comments, may now look like this.

```

NNODE      16
NDIM        2
NDOFMAX     1
TEMPERAT
  TETA       0.9
TINITIAL    20.0
  NMAT       2
ELEMENTS
  SOLID      9
  NG         2
  NVOID      0
END_ELEM

```

SERIES 12: NODES

A. 1 card

COMMAND, choice between two possible settings.

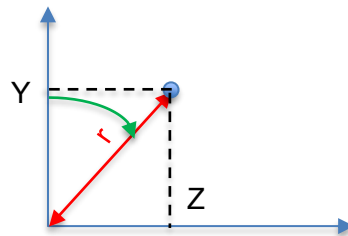
- COMMAND = NODES

The position of the nodes will be given in a Cartesian system of coordinates, see Figure 1.

- COMMAND = NODES_CYL

The position of the nodes will be given in a cylindrical system of coordinates. Cylindrical coordinates are transformed for the internal solution process by the following equations:

$$\begin{aligned} \text{if } ndim = 2 \quad (r, \theta) \Rightarrow \quad & Y = \text{First coord.} = r \cos(\theta) \\ & Z = \text{second coord.} = r \sin(\theta) \end{aligned}$$



$$\text{if } ndim = 3 \quad (r, \theta, Z) \Rightarrow X = r \cos(\theta); Y = r \sin(\theta); Z$$

Note that θ must be introduced in degrees. The transformation is made after all nodes have been read and the automatic generation and repeat have been made, see card C and D.

Several cards are then written, following the format of B, C or D, until all *nnode* nodes have been given their position.

B. 1 card giving the position of 1 node

NODE, *nno*, *rcoordg*(1,*nno*), *rcoordg*(2,*nno*), *rcoordg*(3,*nno*)

- NODE

Command.

- *nno*

Number of the node.

- *rcoordg*(1,*nno*)

First coordinate (in meter) of node *nno*.

- *rcoordg*(2,*nno*)

Second coordinate (in meter or in degree) of node *nno*.

- *rcoordg*(3,*nno*)

Third coordinate (in meter) of node *nno*. Present only if *ndim* = 3.

C. 1 card (optional) for automatic generation

`GNODE, nno, rcoordg(1,nno), rcoordg(2,nno), rcoordg(3,nno)`

- `GNODE`

This command is used for automatic equidistant generation of nodes between the previously defined node and the node *nno*.

- *nno*

Number of the node.

Figure 1: global axes in a Cartesian system of coordinates

- `rcoordg(1,nno)`

First coordinate (in meter) of node *nno*.

- `rcoordg(2,nno)`

Second coordinate (in meter or in degree) of node *nno*.

- `rcoordg(3,nno)`

Third coordinate (in meter) of node *nno*. Present only if *ndim* = 3.

D. 1 card (optional) for repeating a series of nodes

`REPEAT, nno, delta(1), delta(2), delta(3), kgene`

- `REPEAT`

This command is used to repeat the definition of the *nno* previously defined nodes with an increment in each coordinate.

- *nno*

Quantity of nodes to be repeated.

- `delta(1)`

Increment for the first coordinate (in meters).

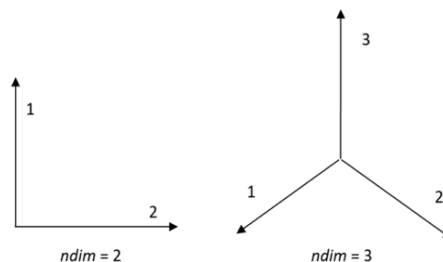
- `delta(2)`

Increment for the second coordinate (in meters or in degrees).

- `delta(3)`

Increment for the third coordinate (in meters). Present only if *ndim* = 3.

- *kgene*



Quantity of times that the previous *nno* defined nodes have to be repeated.

For example, the following series of cards:

NODES				
NODE	1	0.000	0.000	
GNODE	4	0.000	0.120	
REPEAT	4	0.025	0.010	3

is equivalent to:

NODES			
NODE	1	0.000	0.000
NODE	2	0.000	0.040
NODE	3	0.000	0.080
NODE	4	0.000	0.120
NODE	5	0.025	0.010
NODE	6	0.025	0.050
NODE	7	0.025	0.090
NODE	8	0.025	0.130
NODE	9	0.050	0.020
NODE	10	0.050	0.060
NODE	11	0.050	0.100
NODE	12	0.050	0.140
NODE	13	0.075	0.030
NODE	14	0.075	0.070
NODE	15	0.075	0.110
NODE	16	0.075	0.150

The nodes that have been generated are shown on Figure 2.

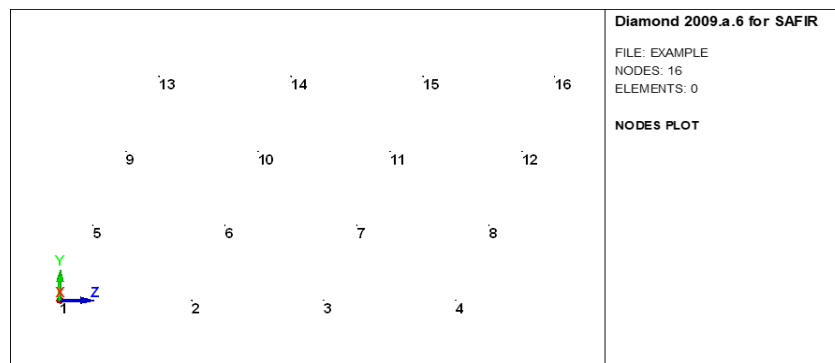


Figure 2: nodes created by GNODE and REPEAT commands

Note: If $ndim = 2$ and the results of a thermal analysis are to be used in the structural analysis of beam elements, then the first coordinate corresponds to the local **y** axis of the beam element and the second coordinate corresponds to the local **z** axis of the beam element.

SERIES 13: NODE LINE

This series is only present if `MAKE.TEM`, `MAKE.TEMHA`, `MAKE.TEMLF`, `MAKE.TEMCD` or `MAKE.TEMTR` has been given in series 9, A.

The values entered in this series will not influence the values of the temperatures that will be calculated. They are relevant only for the structural calculation using the beam elements the section of which is described in the discretization made for the thermal analysis².

A. 1 card

`NODELINE`, Y_0 , Z_0

- `NODELINE`

Command.

- Y_0

First coordinate of the node line in the section of the BEAM finite element.

- Z_0

Second coordinate of the node line in the section of the BEAM finite element.

B. 1 card

`YC_ZC`, Y_C , Z_C

- `YC_ZC`

Command.

- Y_C

First coordinate of the centre of rotation in the section of the BEAM finite element.

- Z_C

Second coordinate of the centre of rotation in the section of the BEAM finite element.

² See Part 3

SERIES 14: IMPOSED TEMPERATURES

A. 1 card

FIXATIONS

Command.

B. 1 card (optional) at each node where the evolution of the temperature as a function of time is imposed by the user.

BLOCK, *nno*, *cblock(nno)*

- BLOCK

Command.

- *nno*

Number of the node where the evolution of the temperature is imposed.

- *cblock(nno)*

Name of the function³ describing the evolution of the temperature at this node (not longer than 10 characters).

C. 1 card (optional) for each master-slave relationship

SAME, *nno1*, *nno2*, YES

- SAME

Command.

- *nno1*

Number of the slave node (its temperature is forced to be equal to the temperature of the master node).

- *nno2*

Number of the master node (a master node can have several slave nodes. A SAME card must be introduced for each slave).

- YES

Command.

D. 1 card (optional) to repeat the previous SAME command

REPEAT, *n*, *incr*, YES

- REPEAT

Command.

- *n*

Quantity of times that the previous SAME command has to be repeated.

- *incr*

Increment on the node numbers *nno1* and *nno2* of the previous SAME command.

- YES

³ See Part 1, Section 5.5

Command.

- E. 1 card (optional) to create master-slave relationship between all nodes that have the same coordinates

SAMEALL, YES

- SAMEALL

Command. All the nodes of the model that have the same coordinates (with a precision of 10^{-8} m) will automatically be attributed a master-slave relationship.

- YES

Command.

- F. 1 card

END_FIX

Command indicating the end of the series.

SERIES 15: SOLID ELEMENTS

- A. 1 card

NODOFSOLID

Command.

Several cards are then written, following the format of B, C or D, until all *nsolid* elements have been described.

- B. 1 card for 1 element

ELEM, *nsol*, *NodesOfSolid*(1,*nsol*), *NodesOfSolid*(2,*nsol*), ... ,

NodesOfSolid(*NumberOfNodesInSolid*,*nno*), *matsolid*(*nsol*), *epsrsolid*(*nsol*)

- ELEM

Command.

- *nsol*

Number of the element.

- *NodesOfSolid*(1,*nsol*)

First node of element *nsol*.

- *NodesOfSolid*(2,*nsol*)

Second node of element *nsol*.

...

- *NodesOfSolid*(*NumberOfNodesInSolid*,*nsol*)

Last node of element *nsol*.

- *matsolid*(*nsol*)

Material number of the element *nsol*. The materials are numbered from 1 to *nmat* according to the order appearing in series 20.

- *epsrsolid(nsol)*

Residual stress (in Pa or N/m²) in element *nsol*. The values entered for *epsrsolid* will not influence the values of the temperatures that will be calculated. They are relevant only for the structural calculation using the beam elements the section of which is described in the discretization made for the thermal analysis⁴. Residual stresses are relevant when *ndim* = 2 and *MAKE.TEM*, *MAKE.TEMHA*, *MAKE.TEMLF*, *MAKE.TEMCD* or *MAKE.TEMTR* have been given in Series 9-A. In other cases, any value can be specified, preferably 0.

If *ndim* = 2, *NumberOfNodesInSolid* = 4.

For triangular elements, *NodesOfSolid*(4,*nsol*) = 0

If *ndim* = 3, *NumberOfNodesInSolid* = 8.

For elements which have a triangular base:

- *NodesOfSolid*(7,*nsol*) and *NodesOfSolid*(8,*nsol*) = 0 for prismatic elements (6 nodes)
- *NodesOfSolid*(5,*nsol*) to *NodesOfSolid*(8,*nsol*) = 0 for tetrahedral elements (4 nodes)

In 2D elements, the nodes must be given in counterclockwise order, see Figure 3. The order of the nodes defines the order of the faces, which will be used to allocate boundary conditions in Series 16 and to define internal cavities in Series 17.

⁴ See User's manual for SAFIR 2022, Part 3

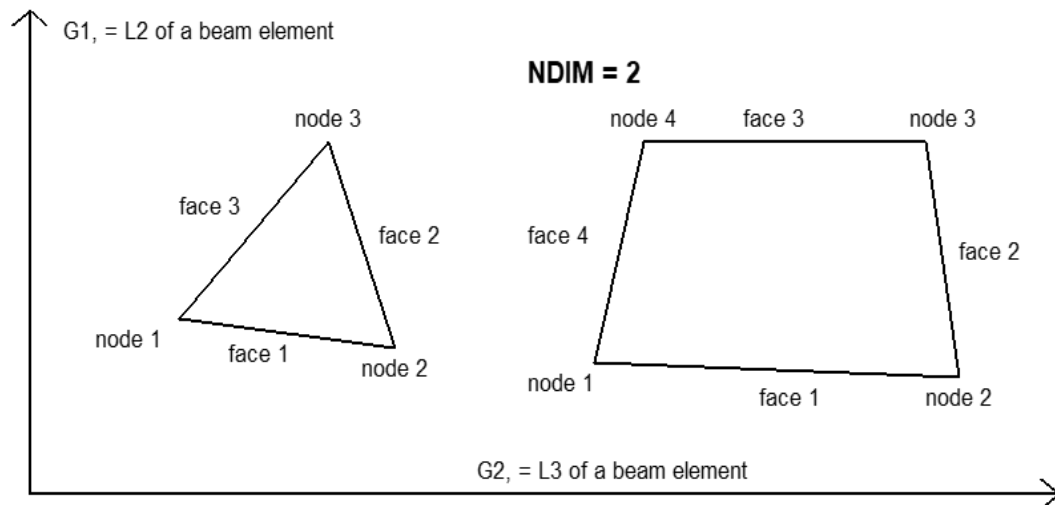


Figure 3: nodes and faces of elements for 2D analyses

In 3D elements with 6 nodes, nodes 1, 2, 3 must belong to one of the triangular faces and nodes 4, 5, 6 to the other one, with the order 1, 2, 3 drilling into the element and 4, 5, 6 drilling out of the element. Node 4 must be on the same edge as node 1, and thus 5 with 2 and 6 with 3, see Figure 4.

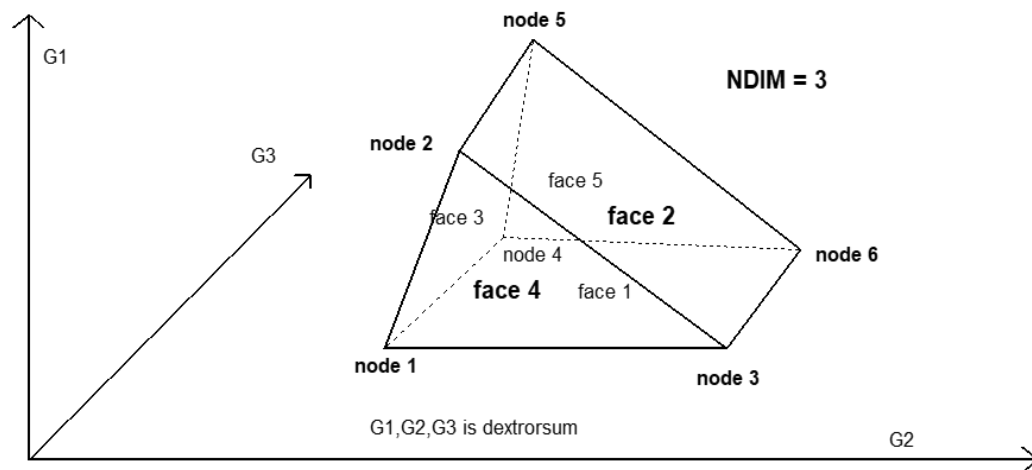


Figure 4: nodes and faces of elements with 6 nodes for 3D analyses

In 3D elements with 8 nodes, nodes 1, 2, 3, 4 must belong to one frontier and nodes 5, 6, 7, 8 to the opposite one, with the order 1, 2, 3, 4 drilling into the element 5, 6, 7, 8 drilling out of the element, see Figure 5. Node 5 must be on the same edge as node 1, and thus 6 with 2, etc.

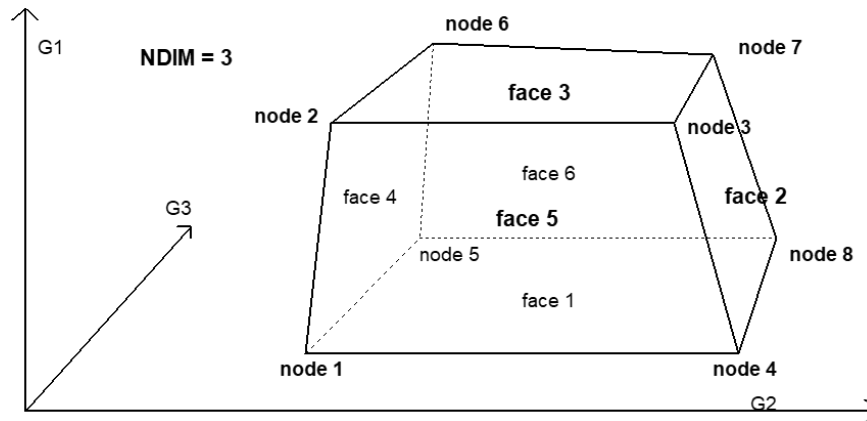


Figure 5: nodes and faces of elements with 8 nodes for 3D analyses

In 3D elements with 4 nodes, nodes 1-2-3 in that order drill into the element; see Figure 6.

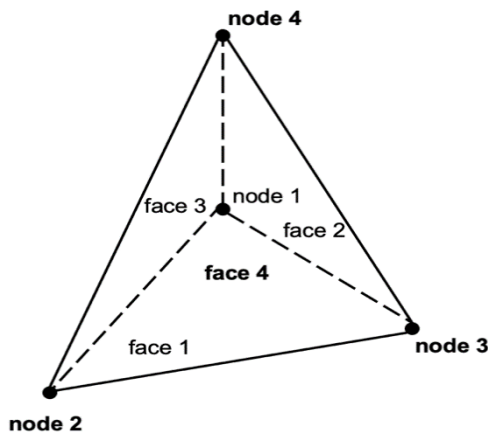


Figure 6: nodes and faces of elements with 4 nodes for 3D analyses

Note: Only hexahedral and octahedral elements can be used in a 3D mechanical analysis. Tetrahedral elements are not supported.

C. 1 card (optional) for automatic generation

GELEM, *nsol*, *NodesOfSolid*(1,*nsol*), *NodesOfSolid*(2,*nsol*), ... ,
NodesOfSolid(*NumberOfNodesInSolid*,*nno*), *matsolid*(*nsol*), *epsrsolid*(*nsol*), *kgene*

- GELEM

Command.

- *nsol*
Number of the element.
- *NodesOfSolid(1,nsol)*
First node of element *nsol*.
- *NodesOfSolid(2,nsol)*
Second node of element *nsol*.
- ...
- *NodesOfSolid(NumberOfNodesInSolid,nsol)*
Last node of element *nsol*.
- *matsolid(nsol)*
Material number of the element *nsol*. The materials are numbered from 1 to *nmat* according to the order appearing in series 20.
- *epsrsolid(nsol)*
Residual stress (in Pa or N/m²) in element *nsol*.
- *kgene*
The elements from the previously defined one up to this one will be generated automatically. *kgene* is the increment of the nodes from one element to the next one.

D. 1 card (optional) for repeating a series of elements

REPEAT, *n*, *incr*, *kgene*

- REPEAT
Command.
- *n*
Quantity of elements to be repeated.
- *incr*
Increment in the node numbers.
- *kgene*
Number of times that the *n* elements have to be repeated.

For example, the following series of cards:

```
FIXATIONS
END_FIX
NODOSOLID
  ELEM    1    1    2    6    5    1    0
  GELEM   3    9   10   14   13    1    0    4
  REPEAT  3    1    2
```

is equivalent to:

```

FIXATIONS
END_FIX
NODOF SOLID
ELEM 1 1 2 6 5 1 0.0000E+00
ELEM 2 5 6 10 9 1 0.0000E+00
ELEM 3 9 10 14 13 1 0.0000E+00
ELEM 4 2 3 7 6 1 0.0000E+00
ELEM 5 6 7 11 10 1 0.0000E+00
ELEM 6 10 11 15 14 1 0.0000E+00
ELEM 7 3 4 8 7 1 0.0000E+00
ELEM 8 7 8 12 11 1 0.0000E+00
ELEM 9 11 12 16 15 1 0.0000E+00

```

It will generate the elements shown on Figure 7.

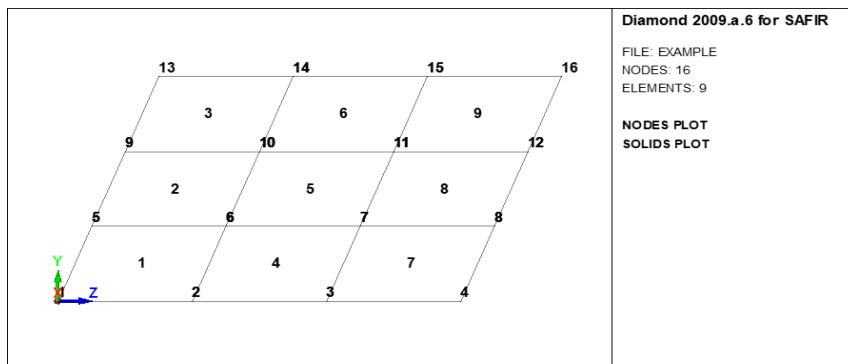


Figure 7: elements created by GELEM and REPEAT

When all elements have been defined, it is possible to change the material of one or several elements. This can be useful if the input file has been created with a text editor and extensive utilization has been made of the `GELEM` and `REPEAT` commands⁵.

E. 1 card (optional) for each element in which the material has to be changed

`NEW_MAT, nsol, matsolid(nsol)`

- `NEW_MAT`

Command.

- `nsol`

Number of the element in which the material must be changed.

- `matsolid(nsol)`

Number of the material to be given to the element `nsol`.

⁵ `NEW_MAT` is typically used to create a steel rebar in a concrete section.

For example, the following series of cards:

NODOSOLID								
ELEM	1	1	2	6	5	1	0	
GELEM	3	9	10	14	13	1	0	4
REPEAT	3	1	2					
NEW_MAT	5	2						

will allocate the materials to the elements as shown on Figure 8 if `STEELEC3EN` is the first material name and `CALCONC_EN`⁶ is the second one, see series 20. Without the `NEW_MAT` command, the description of the elements with the appropriate materials would require 7 cards, instead of 4 cards in the example shown here. The utilisation of the `REPEAT` command would indeed not be possible.

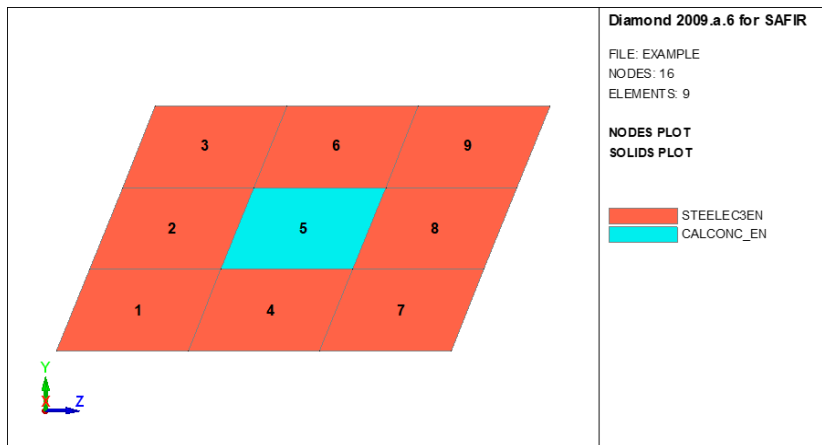


Figure 8: new material assigned

SERIES 16: FRONTIERS

Different cards can be used to allocate boundary conditions to selected surfaces of some elements. Two different boundary conditions can be used:

- either a time-temperature fire curve T_g describes the environment around the model (commands `F` and `GF`). The heat flux q at the boundary will be calculated

⁶ This material is now obsolete and should be replaced by `CONCEN2020`

from the temperature of the fire curve T_g and the temperature on the surface T_s according to Eq. (1):

$$q = h(T_g - T_s) + \sigma \varepsilon (T_g^4 - T_s^4) \quad (1)$$

in which the coefficient of convection h for surfaces exposed to fire (see Series 20 C) will be considered if $T_g > 20^\circ\text{C} + \text{precision}$ (see series 19). If this condition is not fulfilled, the coefficient for surfaces not exposed to fire will be considered. σ is the Stefan-Boltzmann constant ($5.67 \times 10^{-8} \text{ Wm}^{-2}\text{K}^{-4}$) and ε is the relative emissivity of the material at the surface, see Series 20 C.

- or the incipient flux on the model is prescribed (commands `FLUX` and `GFLUX`), either with a value defined by the user, or computed by one of the local fire models (HASEMI, LOCAFI, CFD and TRAFIR).

A. 1 card

FRONTIER

Command

B. 1 card for each element that has at least one surface exposed to a fire curve

F, *nsol*, *cfrontiersolid*(1,*nsol*), ... , *cfrontiersolid*(*NumberOfFrontier*,*nsol*),

- F

Command.

- *nsol*

Number of the element.

- *cfrontiersolid*(1,*nsol*)

Function describing the fire curve on frontier 1 of element *nsol*.

...

- *cfrontiersolid*(*NumberOfFrontier*,*nsol*)

Function describing the fire curve on the last frontier of element *nsol*.

If *ndim* = 2, *NumberOfFrontier* = 4.

For triangular elements, *cfrontiersolid*(4,*nsol*) = NO

If *ndim* = 3, *NumberOfFrontier* = 6.

cfrontiersolid(6,*nsol*) = NO for prismatic elements which have a triangular base

cfrontiersolid(5,*nsol*) = NO, *cfrontiersolid*(6,*nsol*) = NO for tetrahedral elements

The order of the surfaces on the elements is linked to the node numbers.

In triangular elements, see Figure 3,

frontier 1 is from node 1 to node 2,

frontier 2 is from node 2 to node 3,

frontier 3 is from node 3 to node 1.

In quadrangular elements, see Figure 3,
 frontier 1 is from node 1 to node 2,
 frontier 2 is from node 2 to node 3,
 frontier 3 is from node 3 to node 4,
 frontier 4 is from node 4 to node 1.

In 3D elements with 6 nodes, see Figure 4,
 frontier 1 comprises is defined by the nodes 1, 4, 6, 3,
 frontier 2 comprises is defined by the nodes 2, 5, 6, 3,
 frontier 3 comprises is defined by the nodes 1, 2, 5, 4,
 frontier 4 comprises is defined by the nodes 1, 2, 3,
 frontier 5 comprises is defined by the nodes 4, 5, 6.

In 3D elements with 8 nodes, see Figure 5,
 frontier 1 comprises is defined by the nodes 1, 5, 8, 4,
 frontier 2 comprises is defined by the nodes 4, 3, 7, 8,
 frontier 3 comprises is defined by the nodes 2, 6, 7, 3,
 frontier 4 comprises is defined by the nodes 1, 2, 6, 5,
 frontier 5 comprises is defined by the nodes 1, 2, 3, 4,
 frontier 6 comprises is defined by the nodes 5, 6, 7, 8.

In 3D elements with 4 nodes, see Figure 6,
 frontier 1 comprises is defined by the nodes 1, 2, 3,
 frontier 2 comprises is defined by the nodes 1, 3, 4,
 frontier 3 comprises is defined by the nodes 1, 2, 4,
 frontier 4 comprises is defined by the nodes 2, 3, 4.

The function describing the fire curve can be

- one of the SAFIR defined function (e.g. FISO or F20)⁷,
- or a user defined function (not longer than 10 characters) located in a file⁸,
- or the command NO if no fire curve is applied on a particular surface. The meaning of NO is not “remove any previously fire curve”; it is more to be understood as “disregard this information”. For example:

F	5	FISO	FISO	NO	NO
---	---	------	------	----	----

is equivalent to

F	5	FISO	NO	NO	NO
F	5	NO	FISO	NO	NO

⁷ Section 5.5.2 in User’s manual for SAFIR 2022, Part 1

⁸ *Ibid.*, Section 5.5.3

C. 1 card for automatic generation of frontiers from the previously defined element to this one

GF, nsol, cfrontiersolid(1,nsol), ... ,cfrontiersolid(NumberOfFrontier,nsol), kgene

- *GF*

Command.

- *nsol*

Number of the element.

- *cfrontiersolid(1,nsol)*

Function describing the fire curve on frontier 1 of element *nsol*.

...

- *cfrontiersolid(NumberOfFrontier,nsol)*

Function describing the fire curve on the last frontier of element *nsol*.

- *kgene*

Increment on the element numbers.

For example

F	1	FISO	NO	NO	NO	
GF	7	FISO	NO	NO	NO	3
F	1	NO	NO	NO	F20	
GF	3	NO	NO	NO	F20	1

is equivalent to

F	1	FISO	NO	NO	NO	
F	4	FISO	NO	NO	NO	
F	7	FISO	NO	NO	NO	
F	1	NO	NO	NO	F20	
F	2	NO	NO	NO	F20	
F	3	NO	NO	NO	F20	

Figure 9 shows the boundary conditions created by these cards applied on the section that was shown on Figure 7.



Figure 9: Boundary conditions

D. 1 card for each element that has at least one surface exposed to a defined heat flux
`FLUX, nsol, cfrontiersolid(1,nsol), ... ,cfrontiersolid(NumberOfFrontier,nsol)`

- `FLUX`

Command.

- `nsol`

Number of the element.

- `cfrontiersolid(1,nsol)`

Function describing the flux (in W/m²) on frontier 1 of element `nsol`.

...

- `cfrontiersolid(NumberOfFrontier,nsol)`

Function describing the flux (in W/m²) on the last frontier of element `nsol`.

The function describing the flux can be:

- ✓ either one of the SAFIR defined function⁹ (e.g. `F1000`) or a user defined function (not longer than 10 characters) located in a file (e.g. `[myflux.txt]`),
- ✓ or the command `NO` if no flux is applied on a particular surface.

A positive flux means energy introduced in the section.

It is possible to have a flux condition and a fire curve on the same surface.

Each surface of the model heated by a HASEMI local fire must have a `FLUX` command and the function `HASEMI` where appropriate. For example:

```
FLUX    5    NO    NO    HASEMI    NO
```

⁹ See section 5.5 in "Users manual of SAFIR 2022 – Part 1 General considerations"

There is no need to add a frontier F20 on a surface heated by a HASEMI flux (for reemitting energy); it will be automatically added by SAFIR.

Notes:

- 1) If the function HASEMI_FR is used in the FLUX command, the flux as given by the Equations of EN 1991-1-2 is multiplied by 0.85, as indicated in the French National Application Document to EN 1991-1-2..
- 2) A common error made by several users is that they enter the chain of character "HASEMI.TXT" whereas only "HASEMI" is needed in the FLUX command.

Each surface of the model heated by a LOCAFI local fire must have a FLUX command and the function LOCAFI where appropriate. For example:

```
FLUX      5      NO      NO      LOCAFI      NO
```

There is no need to add a frontier F20 on a surface heated by a LOCAFI flux (for reemitting energy). This effect is included in the model.

Each surface of the model heated by a CFD fire described in a transfer file must have a FLUX command and the function CFD where appropriate. For example:

```
FLUX      5      NO      NO      CFD      NO
```

There is no need to add a frontier F20 on a surface heated by a CFD flux (for reemitting energy). This effect is included in the model.

E. 1 card for automatic generation from the previously defined element.

GFLUX, *nsol*, *cfrontiersolid*(1,*nsol*), ... ,*cfrontiersolid*(*NumberOfFrontier*,*nsol*), *kgene*

- GFLUX
Command.
- *nsol*
Number of the element.
- *cfrontiersolid*(1,*nsol*)
Function describing the flux (in W/m²) on frontier 1 of element *nsol*.
- ...
- *cfrontiersolid*(*NumberOfFrontier*,*nsol*)
Function describing the flux (in W/m²) on the last frontier of element *nsol*.
- *kgene*
increment on the element numbers.

F. 1 card

END_FRONT

Command indicating the end of the series.

SERIES 17: VOIDS

The following cards A, B, C and D are repeated *nvoid* times, see series 11-D. If *nvoid* = 0 or *ndim* = 3, this series is skipped.

A. 1 card

VOID

Command.

B. 1 card for each surface of an element that is adjacent to an internal cavity.

ELEM, *nsol*, *frontiersolid*

- ELEM
Command.
- *nsol*
Number of the element.
- *frontiersolid*
Number of the surface of this element that is adjacent to a cavity (valid values are from 1 to 6).

If one element has two surfaces that define a void, two cards must be entered. For example:

ELEM	5	2
ELEM	5	3

C. 1 card for automatic generation from the previously defined element.

GELEM, *nsol*, *frontiersolid*, *kgene*

- GELEM
Command.
- *nsol*
Number of the element.
- *frontiersolid*
Number of the surface of this element that is adjacent to a cavity, see Figure 10.
- *kgene*
Increment on the element numbers. Can be positive or negative.

D. 1 card

END_VOID

Command indicating the end of the cards defining this cavity.

The elements surrounding a cavity can be listed in any order.

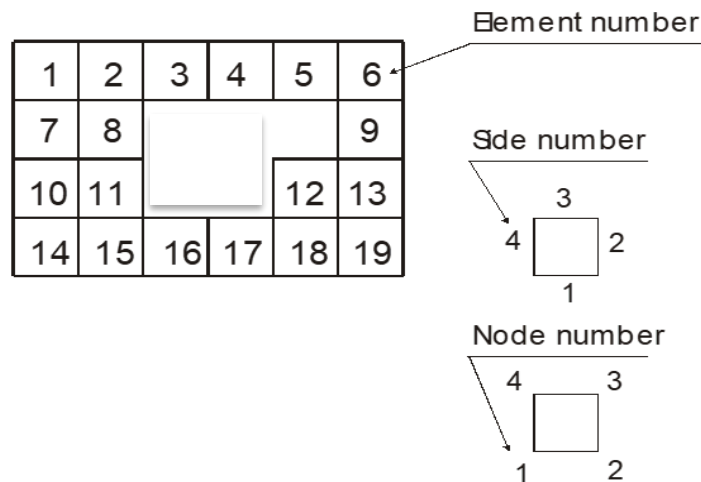


Figure 10; description of a cavity

For example, Figure 10 shows a 2D model with 19 rectangular finite elements and an internal cavity. The cavity can be described by the following cards¹⁰.

¹⁰ In this case, *nfrontiervoid* = 10, see series 11-E.

```

VOID
ELEM    16    3
ELEM    17    3
ELEM    12    4
ELEM    12    3
ELEM     9    4
ELEM     5    1
GELEM    3    1   -1
ELEM     8    2
ELEM    11    2
END_VOID

```

The nodes which determine each surface for other types of elements can be found in the description of series 16-B

Note: For convection inside the cavity, the coefficient of convection on unexposed surfaces is used, irrespective of the temperature of the air in the cavity. This is to account for the low level of turbulence expected to take place in the cavity.

SERIES 18: SYMMETRIES

A. 1 card

SYMMETRY

Command.

The following cards B, C and D are optional. If no symmetry is used when creating the model, only cards A and E are present. Symmetries can only be used in 2D models but this card is nevertheless needed also in 3D models.

B. 1 card for each real axis of symmetry in the section

REALSYM, *nno1*, *nno2*

- REALSYM

Command.

- *nno1*

Number of the first node defining the axis of symmetry.

- *nno2*

Number of the second node defining the axis of symmetry.

The line passing through nodes *nno1* and *nno2* is a real axis of symmetry for the model. This possibility is used when the 2D model represents part of a beam section. When

creating the “.TEM” file, the fibres located on the other side of the axis of symmetry are created, with the same sectional area, same material number and same temperature.

This card can be repeated several times with different successive axes of symmetry. If it is used n times, the section represented in the “.TEM” file will be 2^n times bigger than the one modelled for the thermal analysis.

C. 1 card if the **y** axis is an axis of symmetry in the section.

YSYM

Command.

This card is used if the first axis of coordinate of the model, i.e., the local **y** axis for the beam element, is a thermal and structural axis of symmetry. When creating the “.TEM” file, the area of all fibres is simply multiplied by 2.

This card can only be used when the structural model is a 2D model. Another possible option is not to use the YSYM command and divide the loads applied on the structure by a factor of two¹¹.

The YSYM command can be used simultaneously with one or several REALSYM commands.

D. 1 card if it is desired to analyse a section of 1 meter width.

WIDTH, *width*

- WIDTH

Command.

- *width*

Width of the section. If this command is used, the area of all fibres is divided by *width*. As a result, the section is representative of a section with a width of 1 meter. This command is used essentially for sheet piles or for retaining walls; it allows applying, in the structural analysis, loads on the wall defined per square meter, even if the width of the section represented in the thermal analysis is different from 1 meter.

¹¹ It is even simpler to model the complete section and not to bother about symmetries. This will nevertheless slightly increase the run times and could be an issue when local fire models are used.

E. 1 card for each axis of symmetry in a cavity.

This command is not supported in SAFIR 2025.a.0

`SYMVOID, nno1, nno2, [nno3], nvoid`

- `SYMVOID`
Command.
- `nno1`
Number of the 1st node defining the axis (2D) or the plane (3D) of symmetry.
- `nno2`
Number of the 2nd node defining the axis (2D) or the plane (3D) of symmetry.
- `nno3` (only for 3D models)
Number of the 3rd node defining the plane of symmetry in 3D models.
- `nvoid`
Number of the cavity in which this axis of symmetry must be considered.

This card influences the calculation of the view factors in the cavity; the model as described by the user (and by the eventual previous `SYMVOID` commands) is copied virtually on the other side of the `SYMVOID` axis or plane when computing the view factors. It is theoretically possible to have as much as 4 different `SYMVOID` in a cavity, but the validity of the procedure has been verified only with 2 axes or plane of symmetry in a cavity.

Utilisation of the `SYMVOID` command is only possible if the cavity reconstructed by SAFIR after all `SYMVOID` commands is closed.

If a `SYMVOID` axis is also a real axis of symmetry, a `REALSYM` command must also be defined for this axis to modify the quantity of fibres in the TEM file, see series 18-B.

F. 1 card

`END_SYM`

Command to indicate the end of this series.

SERIES 19: PRECISION

A. 1 card

`PRECISION, precision`

- `PRECISION`
Command.
- `precision`
Small value which must be reached to have convergence.

The value of *precision* is used as a small number at different locations in SAFIR. A good value depends on the type of model that is being analysed and the experience of the

user is useful to choose a good value. 2×10^{-3} is normally acceptable for thermal calculations.

SERIES 20: MATERIALS

A. 1 card

MATERIALS

Command

All *nmat* materials (see Series 10) must be described here. A material is described by:

- a number, from 1 to *nmat*. The number is defined automatically by the order of appearance in the input file, from 1 for the first material to *nmat* for the last one;
- a name, given in cards B. Different materials in a model can have the same name (with the exception of `USERx`, see below). This will be the case if similar materials have different thermal and/or mechanical properties.
- materials properties which depend on the type of material. They are given in cards C.

The descriptions hereafter give the content of cards B and C for the materials that can be used in a thermal analysis.

Note: Many materials require two coefficients of convection, one for heated surfaces, and one for unheated surfaces. For SAFIR, a surface is heated if a FRONTIER condition is applied (see SERIES 16) and the temperature of the gas is greater than 20°C. If one of these two conditions is not met, the coefficient on unheated surface is used.

This can cause unexpected discontinuous behaviour if a physically based fire curve cools down to 20°C, as the coefficient of convection will suddenly change at this time. This can be avoided by either choosing the same value for both coefficients of convection, or cooling the fire down to 21°C.

INSULATION: material with constant thermal properties

B. 1 card

INSULATION

Name of the material.

C. 1 card

$k, c, \rho, w, T_{start}, T_{end}, h_h, h_u, \varepsilon$

- k
Thermal conductivity, in W/mK.
- c
Specific heat, in J/kg K.
- ρ
Specific mass of the dry material, in kg/m³.
- w
Water content, in kg/m³.
- T_{start}
Temperature at which evaporation starts.
- T_{end}
Temperature at which evaporation ends.
- h_h
Coefficient of convection on heated surfaces, in W/m²K.
- h_u
Coefficient of convection on unheated surfaces, in W/m²K.
- ε
Emissivity (no dimension).

Note: T_{start} and T_{end} may be taken as, for example, 100°C and 120°C. Reducing the spread between T_{start} and T_{end} leads to more pronounced plateau in the evolution of the temperature but slows down convergence.

USER_x: material with some thermal properties that vary with temperature.

B. 1 card

USER_x, *ntemperature*

- USER_x
Name of the material. Ten different materials are possible, namely USER₁, USER₂, ... USER₁₀. As an exception to all other material types, only one material number can have the name USER₁, only one material can have the name USER₂, etc.
- *ntemperature*
Quantity of temperatures at which the thermal properties are given. Properties are given at a certain quantity of temperatures, given in increasing order. Linear interpolation is made for intermediate temperatures.
The value of *ntemperature* cannot be smaller than 2.

C. *ntemperature* cards

Card 1

T, k, c, rho, w, Tstart, Tend, h_h, h_c, ε, r

- *T*
First temperature (in degree Celsius) at which thermal properties are given.
- *k*
Thermal conductivity at *T*, in W/mK.
- *c*
Specific heat at *T*, in J/kg K.
- *rho*
Specific mass of the dry material at *T*, in kg/m³.
- *w*
Water content, in kg/m³.
- *Tstart*
Temperature at which evaporation starts.
- *Tend*
Temperature at which evaporation ends.
- *h_h*
Coefficient of convection on heated surfaces, in W/m²K.
- *h_u*
Coefficient of convection on unheated surfaces, in W/m²K.
- *ε*
Emissivity (no dimension).
- *r*
Any positive value (and 0) will force *k, c, rho* to be non reversible. This means that, during cooling from a maximum temperature *T_{max}*, these properties will keep the value that was valid for *T_{max}*. Any negative value will force these properties to be reversible, which means that the value of the property only depends on its current temperature, be it during heating or during cooling.

Card 2 to *ntemperature*

T, k, c, rho

- *T*
Temperature (in degree Celsius) at which thermal properties are given.
- *k*
Thermal conductivity at *T*, in W/mK.
- *c*
Specific heat at *T*, in J/kg K.
- *rho*
Specific mass of the dry material at *T*, in kg/m³.

Take care that the temperatures calculated at the nodes of the model during the iteration process do not go outside the interval of temperatures given by the card N°1 and the card N°*ntemperature*.

As an example, the following 12 cards have been used to represent concrete of EN 1992-1-2, according to the French National Application document¹².

USER1	12									
0.	2.0000	900.	2300.	34.5	100.	120.	25.	4.	0.7	1.
50.	1.8801	900.	2300.							
100.	1.7656	900.	2300.							
115.	1.7323	915.	2300.							
140.	1.6778	940.	2286.							
160.	1.1570	960.	2276.							
200.	1.1108	1000.	2254.							
400.	0.9072	1100.	2185.							
600.	0.7492	1100.	2145.							
800.	0.6368	1100.	2105.							
1000.	0.5700	1100.	2064.							
1200.	0.5488	1100.	2024.							

¹² Equivalent to the material CONCEN2020

GYPSUM: Gypsum plaster boards

B. 1 card

X_GYPSUM or C_GYPSUM

Name of the material.

C. 1 card

h_h, h_c, ε

- h_h

Coefficient of convection on heated surfaces, in W/m²K.

- h_u

Coefficient of convection on unheated surfaces, in W/m²K.

- ε

Emissivity (no dimension).

C_GYPSUM has a 20°C density of 732 kg/m³, whereas X_GYPSUM has a 20°C density of 648kg/m³.

Gypsum type materials lead to a slow convergence of the iterations during the time integration process because of the various peaks in the curve of equivalent specific heat. A time step as small as 1 second may be required.

Sprayed Fire Resistive Material with adjustable thermal properties

SFRM_PROBA is an insulation material with temperature-dependent thermal properties. The thermal properties are based on a probabilistic model calibrated on a NIST study of 3 sprayed fire resistive materials. The details of the probabilistic formulation are taken from: Khorasani N.E., Gardoni P., Garlock M. (2015). "Probabilistic fire analysis: material models and evaluation of steel structural members". *JSE*, 141(12).

A. 1 card

SFRM_PROBA

Name of the material.

B. 1 card

eps_k , eps_c , eps_rho , w , $Tstart$, $Tend$, h_h , h_u , ε

- eps_k

Value of the standard normal parameter ε for the probabilistic evaluation of the temperature-dependent thermal conductivity. A positive (resp. negative) value leads to a conductivity higher (resp. lower) than the average measured experimentally¹³.

- eps_c

Value of the standard normal parameter ε for the probabilistic evaluation of the temperature-dependent specific heat. A positive (resp. negative) value leads to a specific heat higher (resp. lower) than the average measured experimentally.

- eps_rho

Value of the standard normal parameter ε for the probabilistic evaluation of the temperature-dependent specific mass of the dry material. A positive (resp. negative) value leads to a specific mass higher (resp. lower) than the average measured experimentally.

- w

Water content, in kg/m³.

- $Tstart$

Temperature at which evaporation starts.

- $Tend$

Temperature at which evaporation ends.

- h_h

Coefficient of convection on heated surfaces, in W/m²K.

- h_u

Coefficient of convection on unheated surfaces, in W/m²K.

- ε

Emissivity (no dimension).

¹³ See Users manual of SAFIR 2022, Part 5.

CONCRETE of EN 1992-1-2, new generation published in 2020¹⁴:

A. 1 card

CONCEN2020

Name of the material.

B. 1 card

ρ , w , h_h , h_u , ε

- ρ
Specific mass of concrete (including moisture content), in kg/m³.
- w
Water content, in kg/m³.
- h_h
Coefficient of convection on heated surfaces, in W/m²K.
- h_u
Coefficient of convection on unheated surfaces, in W/m²K.
- ε
Emissivity (no dimension).

LIGHT WEIGHT CONCRETE of EN 1994-1-2: 2004

B. 1 card

LWCONC_EN

Name of the material.

C. 1 card

ρ , w , h_h , h_u , ε

- ρ
Specific mass of concrete (including moisture content), in kg/m³.
- w
Water content, in kg/m³.
- h_h
Coefficient of convection on heated surfaces, in W/m²K.
- h_u
Coefficient of convection on unheated surfaces, in W/m²K.
- ε
Emissivity (no dimension).

¹⁴ Latest version : prEN 1992-1-2:2021-09

CONCRETE of EN 1992-1-2: 2004

A. 1 card

CALCONC_EN or SILCONC_EN

Name of the material.

B. 1 card

ρ , w , h_h , h_u , ε , k

- ρ

Specific mass of concrete (including moisture content), in kg/m³.

- w

Water content, in kg/m³.

- h_h

Coefficient of convection on heated surfaces, in W/m²K.

- h_u

Coefficient of convection on unheated surfaces, in W/m²K.

- ε

Emissivity (no dimension).

- k

Parameter that dictates the thermal conductivity λ_c according to the following equation:

$$\lambda_c = \lambda_l + k(\lambda_u - \lambda_l)$$

with

λ_l the lower limit corresponding to curve 2 in Figure 3.7 of EN 1992-1-2;

λ_u the upper limit corresponding to curve 1 in Figure 3.7 of EN 1992-1-2.

CARBON STEEL of EN 1993-1-2: 2005 or EN 1992-1-2: 2004

B. 1 card

STEELEC3EN or STEELEC2EN

Name of the material.

C. 1 card

h_h, h_c, ε

- h_h

Coefficient of convection on heated surfaces, in W/m²K.

- h_u

Coefficient of convection on unheated surfaces, in W/m²K.

- ε

Emissivity (no dimension).

STAINLESS STEEL of EN 1993-1-2: 2005

B. 1 card

STAINLESS

Name of the material.

C. 1 card

h_h, h_c, ε

- h_h

Coefficient of convection on heated surfaces, in W/m²K.

- h_u

Coefficient of convection on unheated surfaces, in W/m²K.

- ε

Emissivity (no dimension).

STAINLESS STEEL of FprEN 1993-1-2: 2023-05

B. 1 card

'SS1.4301', 'SS1.4307', 'SS1.4318', 'SS1.4420', 'SS1.4401', 'SS1.4404',
'SS1.4541', 'SS1.4571' for austenitic stainless steels,
'SS1.4362', 'SS1.4062', 'SS1.4482', 'SS1.4462', 'SS1.4162', 'SS1.4662' for duplex
stainless steels,
'SS1.4509', 'SS1.4521', 'SS1.4621', 'SS1.4003', 'SS1.4016' for ferritic stainless
steels.

Name of the material.

C. 1 card

h_h, h_c, ε

- h_h

Coefficient of convection on heated surfaces, in W/m²K.

- h_u

Coefficient of convection on unheated surfaces, in W/m²K.

- ε

Emissivity (no dimension, 0.4 is the recommended value).

GALVANIZED STEEL:

B. 1 card

GALVASTEEL

Name of the material.

C. 1 card

h_h, h_c

- h_h

Coefficient of convection on heated surfaces, in W/m²K.

- h_u

Coefficient of convection on unheated surfaces, in W/m²K.

The behaviour of GALVASTEEL is the same as that of STEELEC3EN from EN1993-1-2
except that the emissivity is set to 0.35 up to 500°C and then 0.7 for $T > 500^\circ\text{C}$.

ALUMINUM of EN 1999-1-2: 2007

B. 1 card

AL6061_T6, AL6063_T6, AL5083_O, AL5083_H12

Name of the material.

C. 1 card

h_h, h_c, ε

- h_h

Coefficient of convection on heated surfaces, in W/m²K.

- h_u

Coefficient of convection on unheated surfaces, in W/m²K.

- ε

Emissivity (no dimension).

WOOD of EN 1995-1-2: 2004

A. 1 card

WOODEC5

Name of the material.

B. 1 card

ρ , w , h_h , h_c , ε , r , l , m , n

- ρ

Specific mass of wood (including moisture content), in kg/m³.

- w

Water content, in % of the dry mass.

If, for example, $\rho = 450$ kg/m³ and $w = 12$, the density of dry wood is $450 / (1+12/100) = 401.7$ kg/m³

- h_h

Coefficient of convection on heated surfaces, in W/m²K.

- h_u

Coefficient of convection on unheated surfaces, in W/m²K.

- ε

Emissivity (no dimension).

- r

Ratio of conductivity along the grain by conductivity perpendicular to the grain (no dimension), usually greater than 1.

- l, m, n

The vector $\langle l ; m ; n \rangle$ gives the direction of the grain. It does not have to be a length of 1 because it will be normalised to 1 by SAFIR. Direction of the grain is essential for 3D analyses.

Vector components for 2D analysis are given in the order $\langle y ; z ; x \rangle$ with y vertical upward and z horizontal to the right, see Figure 1. Most 2D analyses are performed on the section of a beam or a column and the grain is perpendicular to the section, with a vector $\langle 0 ; 0 ; 1 \rangle$. If grain direction is parallel to z -axis, for example, then the vector should be $\langle 0 ; 1 ; 0 \rangle$.

In 2D models, two different possibilities are thus possible to define an isotropic material:

- ✓ specifying a vector $\langle 0 ; 0 ; 1 \rangle$
- ✓ specify $r = 1$

In 3D models, vector components l , m and n correspond to the axes of the global system of coordinates X , Y and Z

WOOD of prEN 1995-1-2: 2020

A. 1 card

WOOD2020

Name of the material.

B. 1 card

Same as for WOODEC5

SERIES 21: TIME DISCRETIZATION

A. 1 card

TIME

Command.

B. 1 card

Two cases are possible:

- 1) In an **analysis with** COMEBACK, see series 7, a single line must be used because the program adjusts itself the time steps during calculation.

timestep, uptime, timestepmax

- *timestep*
Initial time step in seconds.
- *uptime*
Time for end of the calculation.
- *timestepmax*
Maximum value of the time step.

```
TIME
  2.      3600.      16.
ENDTIME
```

In the example above, the simulation will start with a time step of 2 seconds, and it will vary automatically between a minimum given in the COMEBACK command and a maximum of 16 seconds, depending on the number of iterations that are requested in the successive time steps. The simulation will stop after 1 hour of fire.

- 2) In an **analysis with** NOCOMEBACK, several lines can be given (maximum of *idimtimestep* lines, = 100 in SAFIR2022).
One line added for each time frame added.

timestep, uptime

- *timestep*
Time step in seconds.
- *uptime*
Limit of validity of this time step

TIME	
12 .	3600 .
20 .	7200 .
ENDTIME	

The example above leads to a time step of 12 seconds being used during the first hour, then 20 seconds up to 2 hours, time when the simulation will be stopped.

- C. 1 card, time last line
One line, end of time discretization series.
ENDTIME

Command.

SERIES 22: OUTPUT RESULTS

- A. 1 card
OUTPUT

Command.

- B. 1 card
TIMEPRINT

Command.

- C. at least 1 card, maximum 16 cards

dt, t

- *dt*
Time step (in seconds) used for writing the calculated temperatures in the ".OUT" file and in the eventual ".TEM" or ".TSH" files.
- *t*
Time (in seconds) until which *dt* is used.

D. 1 card

END_TIMEPR

Command to indicate the end of the TIMEPRINT cards.

The following example leads to a time step of 1 minutes being used for writing the temperatures during the first hour, then 15 minutes up 2 hours:

```
OUTPUT
TIMEPRINT
          60.      3600.
          900.     7200.
END_TIMEPR
```

It is recommended to choose the values of dt in accordance with the values of the time steps chosen in series 21 in such a way that the time steps are divisors of the timeprint. The example given above is adequate for the time steps of 12 and 20 seconds mentioned in series 21. The values of 2 and 16 seconds

E. 1 card (optional)

PRINTDEPL, *Tstart*

- PRINTDEPL

Writes the increment of temperatures at each iteration of each time step of the time integration, see series 21. This command is used only for debugging convergence problems or to decide of an appropriate time step for the time integration. It is not used for usual calculations because it slightly increases the run time but, first of all, it increases significantly the size of the “.OUT” file.

- *Tstart*

Time (in seconds) from which the increments of temperature will be written.

F. 1 card (optional)

PRINTFHE, *Tstart*

- PRINTFHE

Writes the out of balance thermal loads at the nodes at each iteration of each time step of the time integration, see series 21. This command is used only for debugging convergence problems or to decide of an appropriate time step for the time integration. It is not used for usual calculations because it slightly increases the run time and it increases significantly the size of the “.OUT” file.

- *Tstart*

Time (in seconds) from which the increments of temperature will be written.

G. 1 card

1 blank line to indicate that the input file is finished.

The example input file given hereafter yields the temperatures calculated after 2 hours shown on Figure 11.

This file has been created as an example for the users manual of SAFIR
 Author: Jean-Marc Franssen

```

      NNODE    16
      NDIM     2
      NDOFMAX   1

      TEMPERAT
        TETA      0.9
      TINITIAL   20.0

      NMAT      2
      ELEMENTS
        SOLID     9
        NG        2
        NVOID     0
      END_ELEM

      NODES
        NODE      1      0.000      0.000
        GNODE     4      0.000      0.120
        REPEAT    4      0.025      0.010      3

      FIXATIONS
      END_FIX

      NODOFSOLID
        ELEM      1      1      2      6      5      1      0.
        GELEM     3      9      10     14     13      1      0.      4
        REPEAT    3      1      2
        NEW_MAT   5      2

      FRONTIER
        F         1      FISO    NO     NO     NO
        GF        7      FISO    NO     NO     NO      3
        F         1      NO      NO     NO     F20
        GF        3      NO      NO     NO     F20      1
      END_FRONT

      SYMMETRY
      END_SYM

      PRECISION   0.002
  
```

TIME	12.	3600.
	20.	7200.
END_TIME		
OUTPUT		
TIMEPRINT	60.	3600.
	900.	7200.
END_TIMEPR		

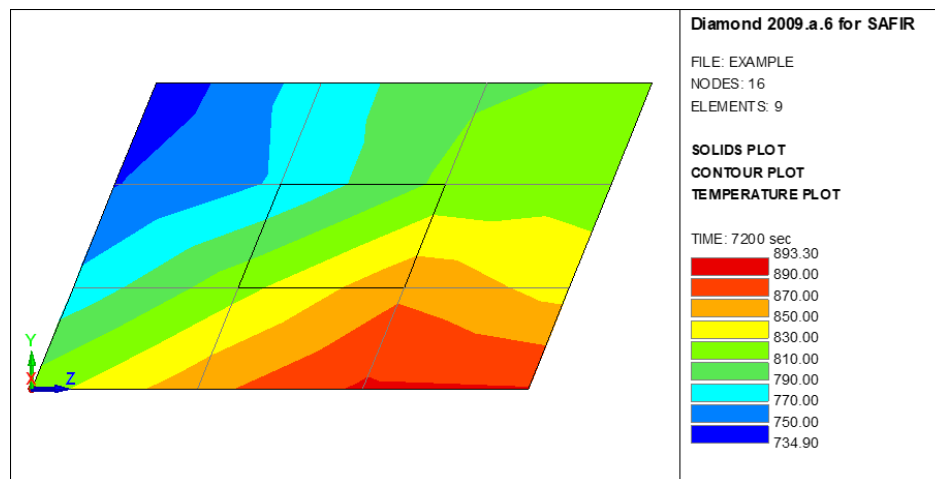


Figure 11: calculated temperatures

2. Detailed description of the file describing the HASEMI fire(s)

If a HASEMI function is used in a FLUX command of the input file, see series 16, a file called “*hasemi.txt*” must be present in the same folder as the input file. This file gives the position and the characteristics of the local HASEMI fire(s).
The format of this is described in this section.

SERIES 1: COMMENTS

A. Multiple cards (can be 0)

As many lines as required may be introduced by the user at the beginning of the file to comment the content of the file. These comments will not influence in any manner the results of the calculation. They will help understand what the file is about, which may be particularly useful if the file is found and opened several years after it has been created.

B. 1 card

1 blank line to indicate that the comments are finished.

SERIES 2: QUANTITY OF FIRE(S)

1 card

NFIRE, *nfire*

- NFIRE

Command.

- *nfire*

Quantity of localised fires that will influence the model in the thermal analysis.

The following series 3 to 6 must be written *nfire* times, once for each localised fire.

SERIES 3: POSITION OF THE FIRE

1 card

FIRE_POS, *posi1*, *posi2*, [*posi3*]

- FIRE_POS
Command.
- *posi1*
Position of the fire along the first axis of coordinates of the structural model.
- *posi2*
Position of the fire along the second axis of coordinates of the structural model.
- *posi3*
Position of the fire along the third axis of coordinates of the structural model.

SERIES 4: CEILING HEIGHT

1 card

HEIGHT, *hc*

- HEIGHT
Command.
- *hc*
Vertical distance from the fire source to the ceiling.
Only this value is present in the local fire model of EN 1991-1-2. It allows detecting whether the flame of the fire touches the ceiling or not. It will thus influence the severity of the attack of the fire on the structure.
The vertical position of the fire given in Series 3 *posi3* is in fact not used in the HASEMI model.

SERIES 5: DIAMETER

A. 1 card

DIAMETER

Command.

B. at least 2 cards, maximum 100 cards

t, diameter

- *t*

Time (in seconds) when the diameter is given. The evolution of the diameter as a function of time will be linearly interpolated between the values given in this series.

- *diameter*

Value of the diameter (in meters) of the fire at time *t*.

C. 1 card

END_DIAM

Command.

SERIES 6: RATE OF HEAT RELEASE

A. 1 card

RHR

Command.

B. at least 2 cards, maximum 100 cards

t, rhr

- *t*

Time when the rate of heat release is given. The evolution of the rate of heat release as a function of time will be linearly interpolated between the values given in this series.

- *rhr*

Value of the rate of heat release of the fire at time *t*.

C. 1 card

END_RHR

Command.

Hereafter is given an example of a “*hasemi.txt*” file.

Description of the local fire by the Hasemi method.

There are 2 local fires.

This file has been used with the structure described in the file TEST.in

NFIRE	2	Quantity of localised fires	
FIRE_POS	0.	0.	0.5
HEIGHT	2.5	Distance between the fire and the ceiling	
DIAMETER			
	0.	0.	Time (s) - Fire source diameter (m)
	300.	3.	
	600.	4.	
END_DIAM			
RHR			
	0.	0.	Time (s) - Rate of heat release (W)
	600.	900000.	
END_RHR			
FIRE_POS	1.5	0.	0.5
HEIGHT	2.5		
DIAMETER			
	0.	0.	
	100.	0.	
	400.	3.	
	600.	4.	
END_DIAM			
RHR			
	0.	0.	
	100.	0.	
	500.	900000.	
	600.	900000.	
END_RHR			

3. Detailed description of the file describing the LOCAFI fire(s)

If a `LOCAFI` function is used in a `FLUX` command of the input file, a file called “*locafi.txt*” must be present in the same folder as the input file. This file gives the position and the characteristics of the local LOCAFI fire(s).

The format of this is described in this section.

SERIES 1: COMMENTS

A. Multiple cards (can be 0)

As many lines as required may be introduced by the user at the beginning of the file to comment the content of the file. These comments will not influence in any manner the results of the calculation. They will help understand what the file is about, which may be particularly useful if the file is found and opened several years after it has been created.

B. 1 card

1 blank line to indicate that the comments are finished.

SERIES 2: QUANTITY OF FIRE(S)

1 card

`NFIRE`, *nfire*

- `NFIRE`

Command.

- *nfire*

Quantity of localised fires that will influence the model in the thermal analysis.

The following series 3 to 6 must be written *nfire* times, once for each localised fire.

SERIES 3: POSITION OF THE FIRE

1 card

FIRE_POS, *posi1*, *posi2*, [*posi3*]

- FIRE_POS
Command.
- *posi1*
Position of the fire along the first axis of coordinates of the structural model.
- *posi2*
Position of the fire along the second axis of coordinates of the structural model.
- *posi3*
Position of the fire along the third axis of coordinates of the structural model.

SERIES 4: CEILING HEIGHT

1 card

Z_CEILING, *Zc*

- Z_CEILING
Command.
- *Zc*
Vertical coordinate of the ceiling.
This value allows detecting whether the flame of the fire touches the ceiling or not. It will thus influence the severity of the attack of the fire on the structure.

SERIES 5: TYPE OF PLUME

1 card

PLUME_TYPE, *plume_type*

- PLUME_TYPE
Command.
- *plume_type*
Gives the type of plume. Can have one of the two following values:
 - ✓ "CYLINDRIC" if the solid flame is a cylinder
 - ✓ "CONIC" if the solid flame is a cone.

SERIES 6: DIAMETER

A. 1 card

DIAMETER

Command.

B. at least 2 cards, maximum 100 cards

t, diameter

- *t*

Time (when the diameter is given. The evolution of the diameter as a function of time will be linearly interpolated between the values given in this series.

- *diameter*

Value of the diameter of the fire at time *t*.

C. 1 card

END_DIAM

Command.

SERIES 7: RATE OF HEAT RELEASE

A. 1 card

RHR

Command.

B. at least 2 cards, maximum 100 cards

t, rhr

- *t*

Time when the rate of heat release is given. The evolution of the rate of heat release as a function of time will be linearly interpolated between the values given in this series.

- *rhr*

Value of the rate of heat release of the fire at time *t*.

C. 1 card

END_RHR

Command.

Hereafter is given an example of a “*locafi.txt*” file.

Description of a local fire following the LOCAFI model.

There is only 1 local fire

NFIRE	1			Quantity of localised fires.
FIRE_POS	0.	0.	0.2	
HEIGHT	3.0			
DIAMETER				
	0.	0.		Time (s) - Fire source diameter (m)
	600.	3.		
	3600.	3.		
END_DIAM				
RHR				
	0.	0.		Time (s) - Rate of heat release (W)
	600.	3534000.		(corresponds to 500 kW/m ²)
	3600.	3534000.		
END_RHR				

4. Detailed structure of the file that describes the TRAFIR compartment.

The concept of travelling fire in SAFIR is the result of an RFCS project, the report of which can be found here:

https://www.steelconstruct.com/wp-content/uploads/TRAFIR_FinalReport_revised.pdf

The first step is to run the specifically written software “TRAFIR4SAFIR” which can be found here:

